

SYSTEM AND METHOD FOR DIFFERENTIAL DATA DETECTION

TECHNICAL FIELD OF THE INVENTION

The present invention is generally related to radio receivers and, more particularly to a system and method for data detection in an angular modulation environment at a low intermediate frequency.

BACKGROUND OF THE INVENTION

Technology has seen an unprecedented ramp-up over the past several years. In our new technological world, the systems that support the technology have become increasingly complex, and the world has become wired. The Bluetooth wireless local area network operates to eliminate those wires.

The Bluetooth wireless LAN system has been in existence for a number of years now, but it is just beginning to garner a great deal of attention from the corporate world. The wireless LAN system as implemented allows everyday devices to communicate with each other on “scatternets.” In brief, a scatternet is a sort of amorphous network. The devices connected to the network constantly change because of their mobile nature, and the mobile nature of the network itself. Each network device has the capability to be either a master or a slave, and sometimes both at the same time.

The network devices communicate with each other via a radio frequency (RF) connection. First generation Bluetooth devices use a spread spectrum frequency hopping (SSFH) technique in the 2.4GHz, Industrial, Scientific, and Medical (ISM) frequency range. This supports a data transfer rate of around 1Mbps. Further, the frequency hopping nature of the network also makes it difficult to intercept the transmissions,

because the transmission frequency is constantly hopping in accordance with a hopping sequence known to both of the network devices and set based on the clock signal of the master device.

As such, the radio transmitters and receivers of these devices need to be very complex. The receiver comprises both a radio portion and a data detection portion. Data detection comes in many different forms. However, most of the existing data detection methods create problems in terms of either power consumption and/or cost efficiency. It is to that end that the present invention is aimed, i.e. performing data detection in a way that reduces power consumption requirements and that is cost efficient.

SUMMARY OF THE INVENTION

The invention involves a data detector, for generating a data signal from a radio frequency input signal stream. The data detector comprises delay logic, first multiplication logic, second multiplication logic and an adder. The delay logic receives an unfiltered input signal having quadrature and in-phase components, and applies a delay to each of the in-phase and quadrature phase components of the unfiltered input signal. The first multiplication logic then multiplies the delayed in-phase component of the unfiltered input signal by the quadrature phase component of the unfiltered input signal to obtain a first multiplication result. The second multiplication logic multiplies the delayed quadrature phase component of the unfiltered input signal by the in-phase component of the unfiltered input signal to obtain a second multiplication result. Finally, an adder adds the first multiplication result with the second multiplication result and generates a decision signal.

Another embodiment of the delay logic of the data detector receives an input signal in quadrature and in-phase components, and applies a delay to each of the in-phase and quadrature phase components of the input signal, wherein the delay is adjustable, allowing for frequency offset compensation. Then, the first multiplication logic multiplies the delayed in-phase component of the input signal by the quadrature phase component of the input signal to obtain a first multiplication result, and a second multiplication logic multiplies the delayed quadrature phase component of the input signal by the in-phase component of the input signal to obtain a second multiplication result. Finally, an adder adds the first multiplication result with the second multiplication result to generate a decision signal.

The invention also comprises a method for detecting data in a radio frequency signal stream. An unfiltered input signal having an in-phase component and a quadrature phase component is received, and the in-phase and quadrature phase components of the input signal are delayed. Then, the in-phase component of the input signal is multiplied by the delayed quadrature phase component of the input signal to yield a first multiplication result. The delayed in-phase component of the input signal is multiplied by the quadrature phase component of the input signal to yield a second multiplication result. Finally, the first and second results are summed to generate a decision signal, which represents a data stream.

These and other features and advantages of the present invention will become apparent from the following description, drawings and claims.

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DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENT

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input band selection filter 105 uses its knowledge about the incoming signal to filter out the desired signal from everything else that may be travelling in the same general frequency range.

After the unwanted signals have been filtered from the desired signal, a low noise amplifier 110 is applied to the signal. The low noise amplifier 110 amplifies the signal and only adds a relatively small amount of noise to the signal.

Next, after the low noise amplifiers 110, the signal is split and fed into separate mixing devices 120, 121, which quadrature convert the signal to a low intermediate frequency (IF) period. In this application, local oscillators (LO) 120, 121 perform the quadrature conversion of the signal. These LO mixing devices 120, 121 are generally used in super heterodyne systems for mixing an analog signal with the incoming radio frequency signal before the data is removed from the signal. The quadrature conversion results in an in-phase component of the signal and a quadrature phase component of the signal. The in-phase component is regarded as the real portion of the signal, whereas the quadrature component is regarded as the portion of the signal lying along the imaginary axis.

Next, the separate signals (in-phase and quadrature phase) are separately fed into an AC coupling devices 130, 131, such as capacitors, where the DC component of the signal is removed. The signals then each go through a complex domain (poly-phase) channel selection filter 140. The filter 140 in this example consist of five stages, but in alternative embodiments can be any number of stages, each implementing a complex pole followed by a gain. The overall transfer function of the filter 140 follows approximately the Butterworth or bandpass filter characteristic with a bandwidth of about 1MHz, in this

example, but could be numerous other types of filters, depending on the implementation. The IF frequency on the front end is chosen according to the needs of the complex domain filter 140. There is a balancing performed between 1/flickernoise (1/f noise) and the filter requirements. Higher frequencies lower the 1/f noise, but increase the complexity and power consumption of the complex domain filter 140. Here, for example, the IF frequency was chosen to be 2MHz, which is high enough to avoid most of the adverse effects of 1/f noise, while low enough so that the required Q-factors in the filter are still practical. However, one skilled in the art should recognize that the choice of IF frequency is ultimately a matter of preference depending on the user and on the application.

The filtered signals are then amplified by amplifiers 150, 151, and sampled and limited by hard limiters 160, 161 prior to the signals entering the data detector 180. In some of the drawings, these three functions have been combined into a single block shown as a square wave with a sampling frequency applied. In the present drawing, the sampling and limiting functions have been combined into blocks 160 and 161. The limiting elements 160, 161 basically square-off the signals. In other words, the highest and lowest amplitudes of the signal are clipped, such that the signal appears to be a square wave. In Bluetooth, the signal is a Gaussian frequency shift keyed (GFSK) signal, GFSK is a known form of digital frequency modulation. This particular form of frequency modulation shifts the transmitted frequency up a nominal amount to represent a "1" and shifts down a nominal amount to represent a "0." Because the signal is frequency modulated, the amplitude of the signal can be cut without harming or altering the data carried by the waveform.

Finally, both signal components are directed into the data detector 180. Data detectors 180 exist in many forms, and differential detection in particular has been used in many contexts. Binary differential detection of frequency modulated signals have been used in the past, but most of those receivers apply a super heterodyne front end that translates a signal down to a relatively high intermediate frequency, which makes the full integration of the image-reject and channel selection filters impractical. Low IF architectures, however, enable low cost, full integration while avoiding direct conversion problems, such as, for example, DC offset and $1/f$ noise. However, because of the low IF frequency, differential detection of binary frequency modulation is difficult. However, the present embodiment produces a differential detection structure that is suitable for application in low IF environments, and is fully integrated, leading to a cost effective solution for the GFSK receiver.

Differential detection in the traditional sense works by multiplying a signal with a delayed version of itself. The signal is generally delayed by a $\pi/2$ phase shift and a time delay of one symbol period. However, the differential detector poses several problems in a low IF structure with limiting amplifiers. First, creating a phase shift of $\pi/2$ over the whole band width is problematic at low frequencies. Generally a $\pi/2$ phase shift is achieved by adding a delay of 90° to a signal to achieve a $\pi/2$ phase shift at that frequency. The problem is that at low frequencies when a 90° delay is applied, the band over which that delay corresponds to a $\pi/2$ phase shift is very small. In practice, an expensive poly-phase filter with many poles is typically used in order to achieve a $\pi/2$ phase shift across a band of frequencies. The second problem is that double frequency terms appear in differential receivers at low frequencies, and they cannot adequately be

removed, causing a degradation of the detector performance. The final problem is that limiting the signal will produce harmonics that are located very close together, causing interference.

To solve these problems, the data detector 180 of the present invention first eliminates the $\pi/2$ phase shift. Because both in-phase and quadrature phase components were available in the received signal, the $\pi/2$ phase shift is unnecessary. The quadrature phase component of the signal is a 90° shift of the in-phase signal, and thus the quadrature phase component will suffice as the $\pi/2$ shifted portion of the signal. Further, although a finite impulse response filter (FIR) is generally used to remove unwanted harmonics from a signal before performing the differential detection, in accordance with the present invention, it was discovered that the problematic terms can be handled by referring to the mathematics involved in producing the signal:

$$I(t) = A \sum_n \frac{\cos\{(2n+1)[2\pi f_c t + \phi(t)]\}}{2n+1}$$

$$Q(t) = A \sum_n \frac{\sin\{(2n+1)[2\pi f_c t + \phi(t)]\}}{2n+1}$$

$$I_d(t) = A \sum_n \frac{\cos\{(2n+1)[2\pi f_c t + \phi(t-T)]\}}{2n+1}$$

$$Q_d(t) = A \sum_n \frac{\sin\{(2n+1)[2\pi f_c t + \phi(t-T)]\}}{2n+1}$$

wherein the $I_d(t)$ and $Q_d(t)$ terms are the delayed signals, being delayed by one period, T , and the information transmitted is contained within the phase term $\phi(t)$. After multiplying the in-phase signal by the delayed quadrature phase signal and the delayed in

phase signal by the quadrature phase signal, the results are summed, and the decision variable can be expressed as:

$$D(t) = I(t)Q_d(t) - Q(t)I_d(t)$$

which expands to:

$$D(t) = A^2 \sum_n \frac{\sin\{(2n+1)[\phi(t) - \phi(t-T)]\}}{2n+1}$$

The final signal also includes some odd order cross-frequency terms and some signal noise. More importantly, one should appreciate that the even order cross frequency terms have canceled out. Finally, it should be pointed out that the summation term yields the equivalent of a Fourier series of a triangular wave, and as such, the detector has an S-curve with a linear characteristic. This type of curve is particularly appealing in the data detection application because of the ease with which the decision can be made on such a curve.

Referring now to FIG. 2, it can be seen that the incoming in-phase and quadrature phase signals pass through respective amplifiers 200, 201, and then through respective limiters 202, 203 where they are then limited and then sampled by samplers 204, 205, all of which is repeated from the previous drawing for clarity. After sampling, the signal is then split, one for use for the phase shift and time delay produced by delay elements 206, 207, the other for use as the reference signal. The delays elements 206, 207 in the present embodiment are preferably implemented using shift registers 206, 207. These shift registers 206, 207 shift data in and delay it one clock cycle. Alternatively, D flip-flops could be used for this purpose, or one could even use a processor such as a DSP that delays the signal.

The sampling rates on these delay elements 206, 207 are an important factor in the operation of the data detector 180. A high sampling rate would necessitate high speed requirements, thereby increasing power consumption at the detector input stage. Too low of a sampling rate would cause alias effects, which becomes important when considered in conjunction with the limiting operation, which causes harmonic byproducts. In the present example embodiment, a sampling rate of about 50 million samples per second (MSPS) was chosen. However, the exact sampling rate selected depends on the specific operating environment.

The outputs of the delay elements 206, 207 are then sent to multipliers 208, 209 where they are cross multiplied. The cross multiplication performed by multiplication elements 208, 209 entails multiplying the delayed quadrature phase signal by the in-phase signal, and the delayed in-phase signal by the quadrature phase signal. The results of the cross multiplication 208, 209 are then fed into an summing element 210, to produce the decision signal. The sum of the multiplication results is then sent through a post detection filter 211, which removes the remaining IF frequency aliasing terms.

An alternative embodiment of the present invention is illustrated in FIG. 3. Here, the input stage amplifying, limiting and sampling elements shown in FIG. 1 as two sets of elements are combined into a single set of elements 320, 321, with a sampling frequency of "F_{sampling}" 322. However, this change is non-substantive. One skilled in the art would appreciate that the substantive change in this embodiment is that it uses multiple delay elements 324-333. These multiple delay elements 324-333 are used so that the data detector can adjust the delay period. Adjusting the delay period, helps the receiver in receiving a transmission that has been subjected to something that has caused variance in

the frequency offset, such as the operating environment, transfer clock irregularities, etc. Delay selectors 334, 335 choose which signal will be fed into the multiplication elements 336, 337, to be multiplied by its counterpart undelayed signal. After multiplication, the signal is summed in summer 338, and fed through a post detection filter 339.

5 In one embodiment, for example, among others, the adjustable delay can be implemented in two stages. In this situation, the data detector 180 would adjust the delay during the preamble, which is received at the beginning of every packet transmission. The first stage could be a rough compensation adjustment where the decision variable would be tested to see whether it hits a lower or higher threshold a certain number of times. When the threshold is hit a certain number of times, the delay is adjusted to re-center the decision variable. The last stage could be a fine compensation at the end of the preamble, for one example, among others. Here the DC offset would be measured and then used to give the decision variable a proper offset. However, it should be understood by one skilled in the art that there are other frequency offset compensation algorithms that can be substituted for the example of the frequency offset compensation outlined above, which uses an adjustable delay to provide the offset compensation.

Used in conjunction with the differential data detector embodiments described above, a post data correction algorithm as shown in FIG. 4 can be employed after the data detector 180 to provide several decibels of improvement in the sensitivity of the receiver.

20 Inter-symbol interference, which is inherently present in the GFSK modulation technique, is the cause of most of the errors seen in systems that employ this modulation technique. In addition to the Gaussian filter, the complex-domain channel selection filter contributes to inter-symbol interference. This interference is most disruptive in alternating bit

patterns such as 1-0-1-0. In order to minimize the inter-symbol interference, in accordance with the present invention, a simplified implementation of an equalizer is used to reduce the effects of inter-symbol interference.

Referring now to FIG. 4, shown is the differential detector of FIG. 3 used in conjunction with a post detection correction algorithm. In the example implementation of the post detection correction algorithm shown here, a two-input multiplexer 409 is used. The first input is simply the decision signal 410 from the data detector 180. The second input is a feedback signal 411. The feedback signal is delayed by delay element 412 and inverted by inverter 413, such that the feedback signal is an inversion of the previous output of multiplexer 409. The first input to multiplexer 409 is selected and output when the absolute value 415 of the decision variable exceeds a certain threshold value 416. The absolute value 415 of the decision variable is then tested by test element 416. If the absolute value 415 does not exceed a threshold value 417 fed into the test element 416, the previous signal 412 inverted by inverter 413 is selected and output as output signal 414.

In other words, when the decision variable is not clearly indicating one level or another, the level opposite of the previous level is chosen. If a strong high output is indicated, then as long as it remains a strong high, the output of the multiplexer remains high. If the strength of the signal dips below a threshold, then the algorithm assumes that a transition was intended, and switches to output a low signal, the opposite of the previous output. If the signal remains weak, the algorithm again assumes a transition was intended and switches back to a high output. Otherwise, if the signal becomes a strong

low, above the threshold strength, then the output signal will remain low until the signal becomes a weak low, at which time the algorithm will transition to a high output.

The invention outlined herein can be implemented in hardware, software, or any combination thereof, but it should be emphasized that the above-described embodiments of the present invention, particularly, any “preferred” embodiments, are merely possible examples of implementations, merely set forth for a clear understanding of the principles of the invention. Many variations and modifications may be made to the above-described embodiments of the invention without departing from the scope of the invention. All such modifications and variations are intended to be included herein within the scope of this disclosure and the present invention.

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